

Supporting Information

High-Temperature Dielectric Energy Storage Materials Fabricated by Crosslinking Titanium Dioxide and Polyarylene Ether Nitrile

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Finite element Calculation Simulation: The phase field simulation for evolution of conductive channel was conducted as previously reported. A dimensionless phase field variable $s(x, t)$ was introduced to characterize the breakdown state of the materials, where the value of s varies from 0 to 1, representing the undamaged state ($s=1$) and the completely breakdown state ($s=0$), respectively. When it was in any of the middle states, the dielectric constant ϵ_r can be calculated as follows:

$$\epsilon(s) = \frac{\epsilon_0}{f(s) + \eta} \quad (\text{Eq. S1})$$

where $f(s) = 4s^3 - 3s^4$. ϵ_0 is the initial ϵ_r , and η is set as 0.001.

Integrating the entire space Ω occupied by the dielectric gives the energy function of the system:

$$\Pi[s, \Phi] = \int_{\Omega} \left[-\frac{\epsilon(s)}{2} \nabla \Phi \cdot \nabla \Phi + \Gamma \frac{1-f(s)}{l^2} + \frac{\Gamma}{4} \nabla s \cdot \nabla s \right] dV \quad (\text{Eq. S2})$$

where Γ and Φ is breakdown energy, and electric potential, respectively. When the electrostatic energy required to extend the conductive branch per unit length is more than the minimum energy Γ required for breakdown, a conductive channel emerges and propagates. The breakdown failure process is represented by a law of linear dynamic supposing the ratio of damage rate to energy driving force:

$$\frac{\partial s}{\partial t} = -\frac{m \delta \Pi}{\delta s} \quad (\text{Eq. S3})$$

Thus, the evolution equation for the damage variable s can be obtained after substituting in the detailed forms of the energy functions:

$$\frac{1}{m} \frac{\partial s}{\partial t} = \frac{\varepsilon'(s)}{2} \nabla \Phi \cdot \nabla \Phi + \frac{\Gamma}{l^2} f'(s) + \frac{\Gamma}{2} \nabla^2 s \quad (\text{Eq. S4})$$

where, the mobility m is used to characterize the damage diffusivity in composite. To facilitate numerical calculation, we will normalize all lengths by l , energies by Γl , time by $m\Gamma l$, and electric potentials by $\sqrt{\Gamma/\varepsilon^0}$. the resulting dimensionless governing equations:

$$\bar{\nabla} \cdot \left[\frac{1}{f(s)+\eta} \bar{\nabla} \bar{\Phi} \right] = 0 \quad (\text{Eq. S5})$$

$$\frac{\partial s}{\partial t} = - \frac{f'(s)}{2|f(s)+\eta|} \bar{\nabla} \bar{\Phi} \cdot \bar{\nabla} \bar{\Phi} + f'(s) + \frac{1}{2} \bar{\nabla}^2 s \quad (\text{Eq. S6})$$

In which the symbols with over-bars are the dimensionless counterparts of the corresponding quantities.

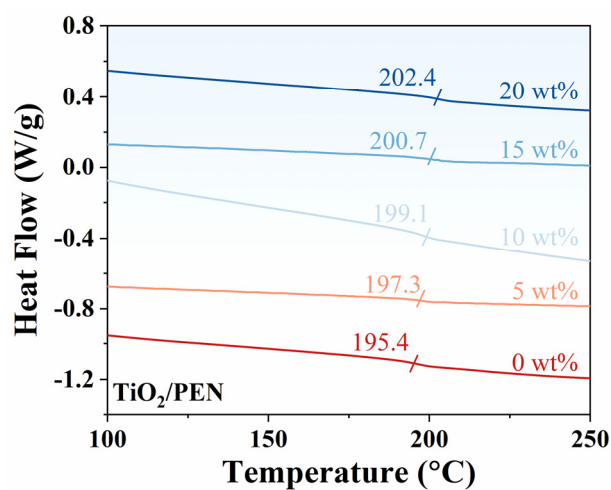


Figure S1. DSC curves of TiO₂/PEN nanocomposites.

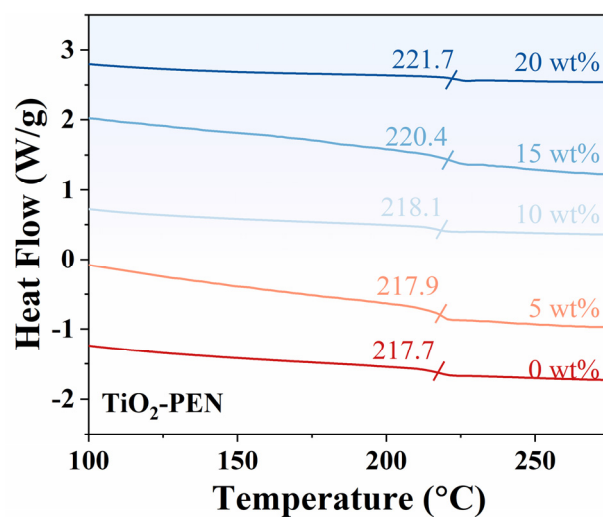


Figure S2. DSC curves of TiO₂-PEN hybrids.

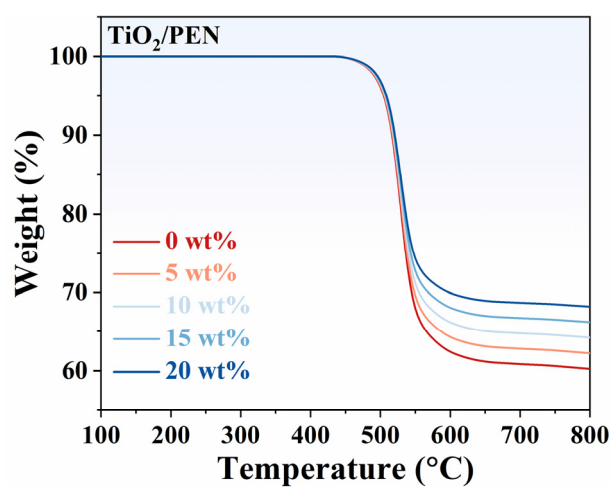


Figure S3. TGA curves of TiO₂/PEN nanocomposites.

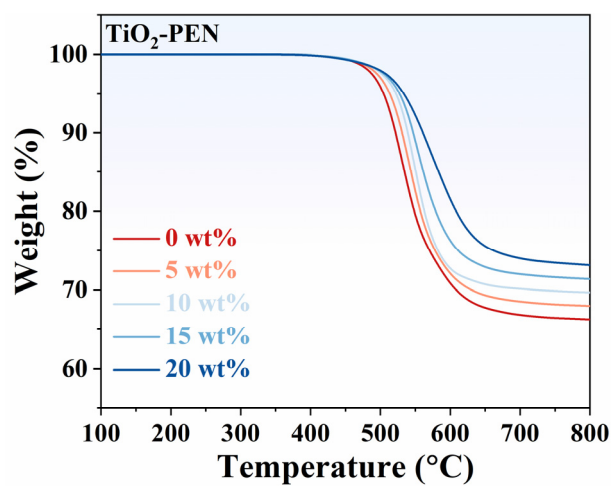


Figure S4. TGA curves of TiO₂-PEN hybrids.

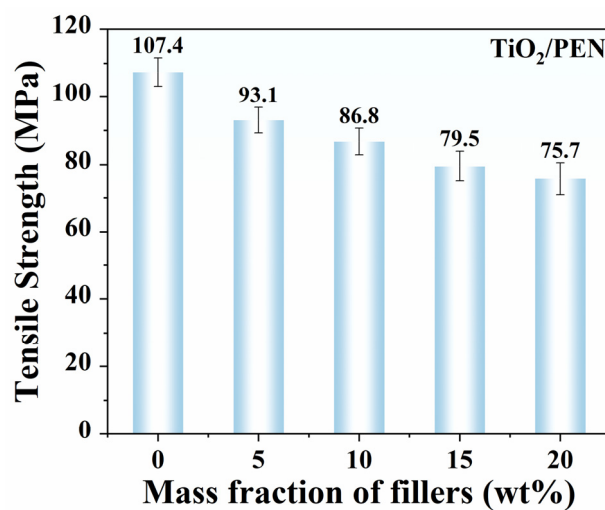


Figure S5. Tensile strength of TiO₂/PEN nanocomposites.

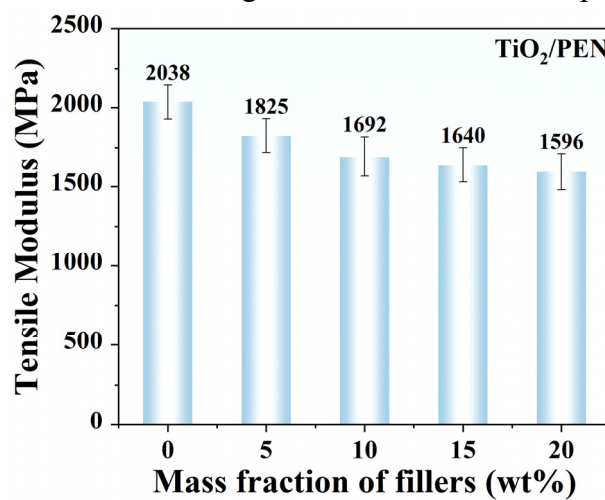


Figure S6. Tensile modulus of TiO₂/PEN nanocomposites.

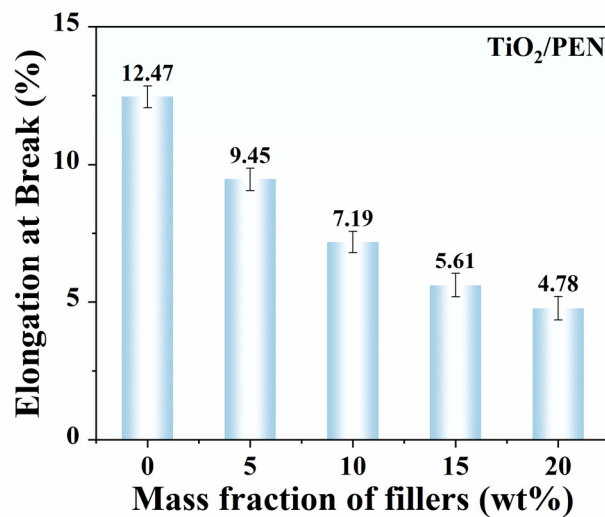


Figure S7. Elongation at break of TiO_2/PEN nanocomposites.

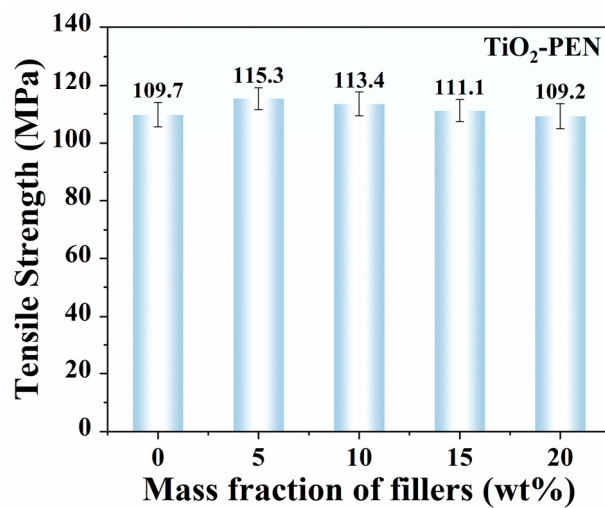


Figure S8. Tensile strength of $\text{TiO}_2\text{-PEN}$ hybrids.

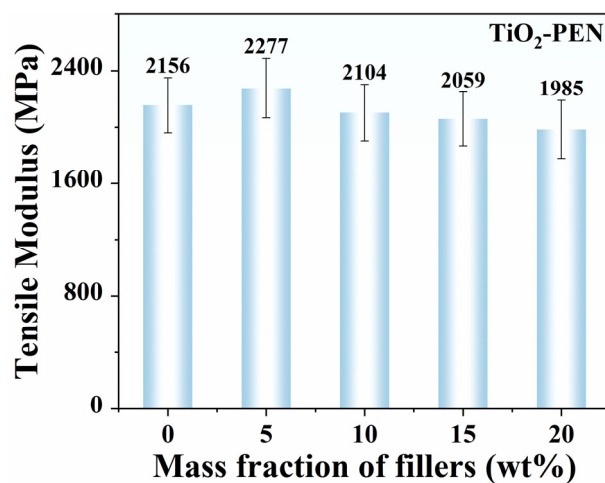


Figure S9. Tensile modulus of $\text{TiO}_2\text{-PEN}$ hybrids.

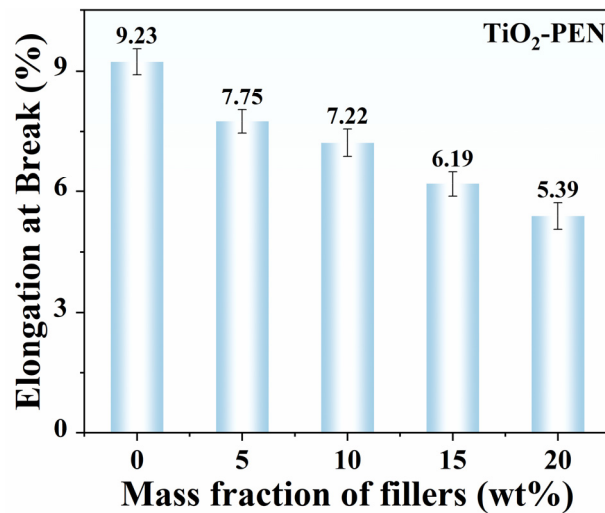


Figure S10. Elongation at break of TiO₂-PEN hybrids.

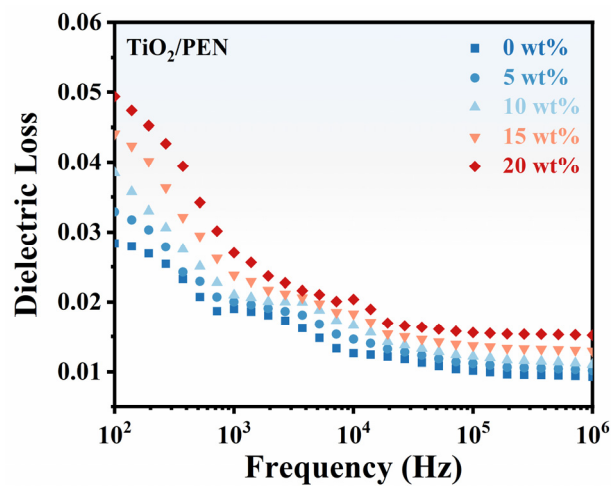


Figure S11. Dielectric loss of TiO₂/PEN nanocomposites.

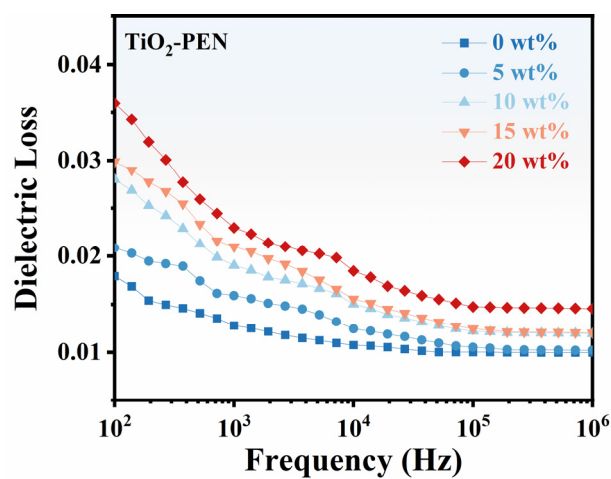


Figure S12. Dielectric loss of TiO₂-PEN hybrids.

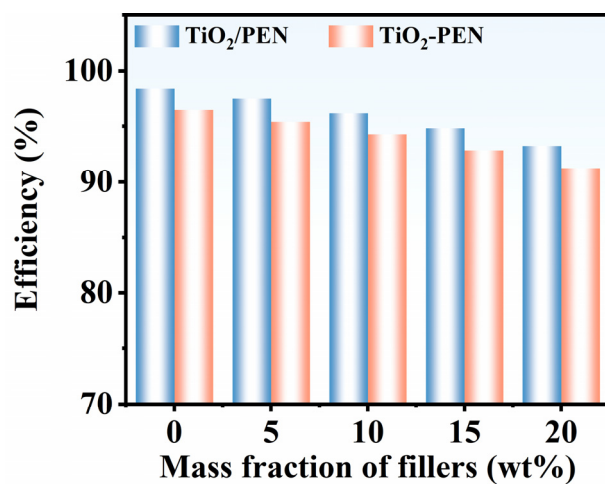


Figure S13. Efficiency of TiO₂/PEN nanocomposites and TiO₂-PEN hybrids.

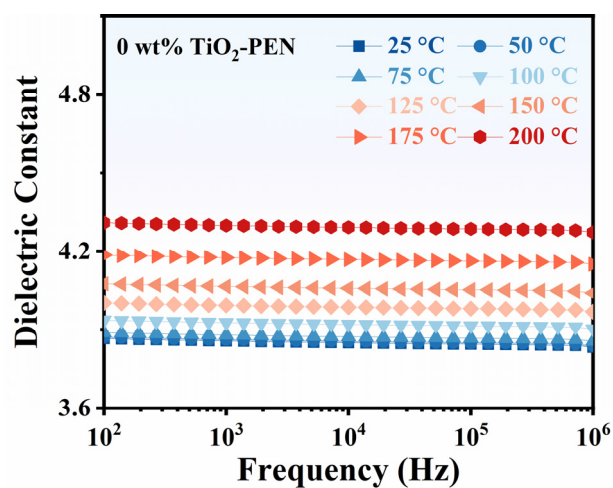


Figure S14. Dielectric constant of 0 wt% TiO₂-PEN at different temperatures.

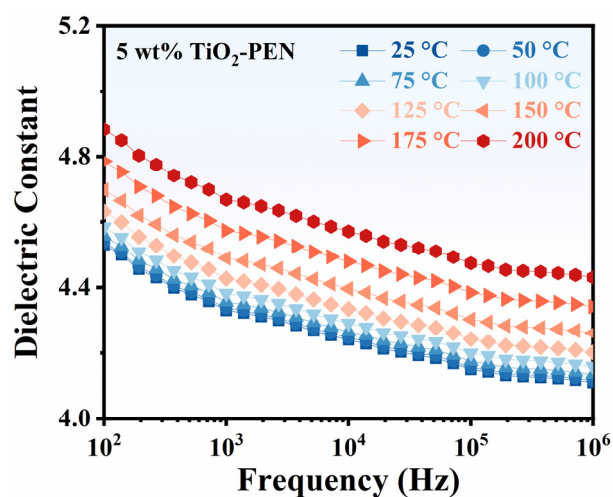


Figure S15. Dielectric constant of 5 wt% TiO₂-PEN at different temperatures.

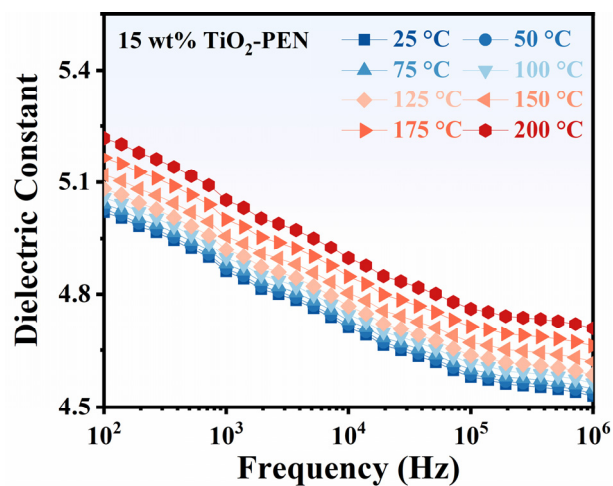


Figure S16. Dielectric constant of 15 wt% TiO₂-PEN at different temperatures.

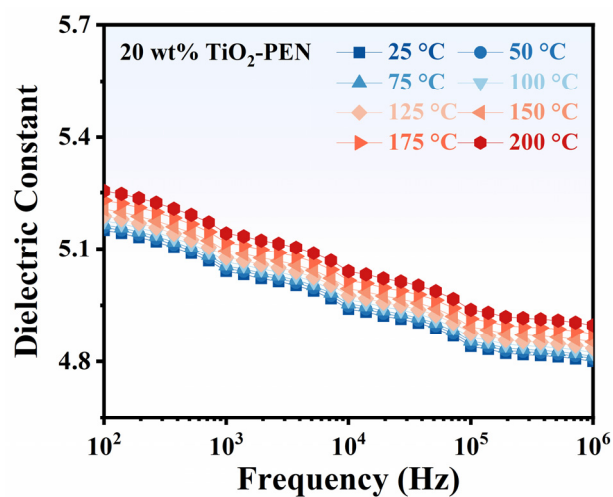


Figure S17. Dielectric constant of 20 wt% TiO₂-PEN at different temperatures.

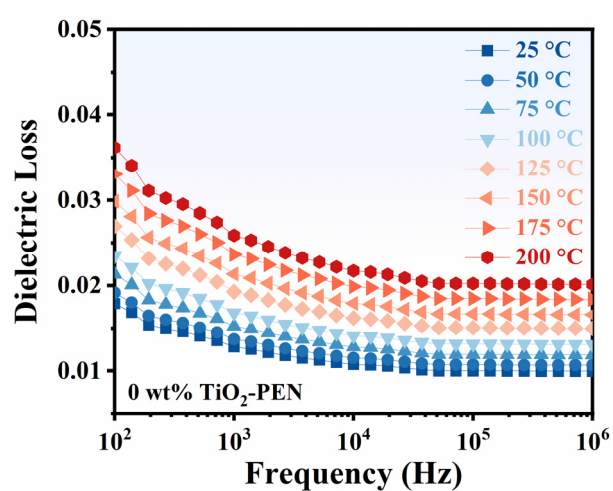


Figure S18. Dielectric loss of 0 wt% TiO₂-PEN at different temperatures.

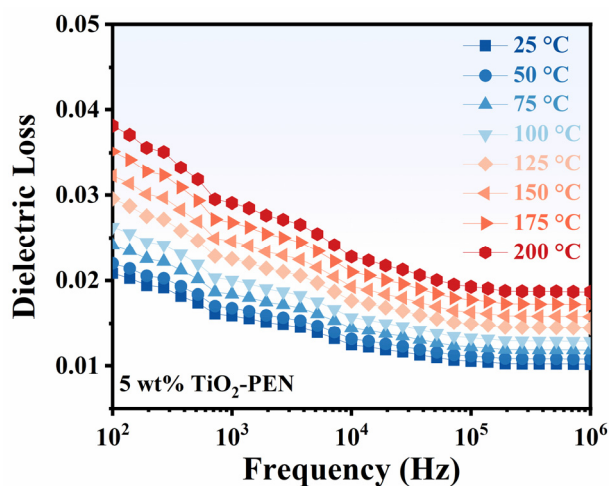


Figure S19. Dielectric loss of 5 wt% TiO₂-PEN at different temperatures.

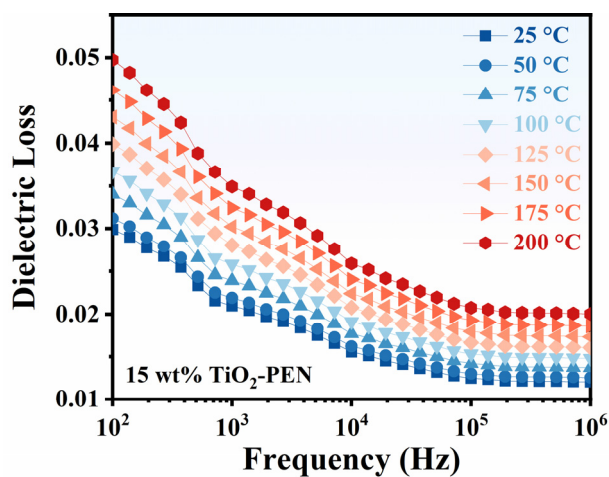


Figure S20. Dielectric loss of 15 wt% TiO₂-PEN at different temperatures.

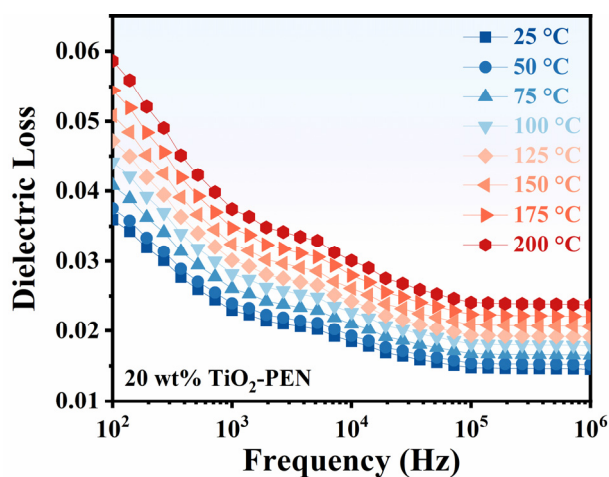


Figure S21. Dielectric loss of 20 wt% TiO₂-PEN at different temperatures.

Table S1. Properties of TiO₂/PEN nanocomposites.

	0 wt%	5 wt%	10 wt%	15 wt%	20 wt%
Glass transition temperature (T _g , °C)	195.4	197.3	199.1	200.7	202.4
Decomposition temperature (T _{10%} , °C)	516.7	517.7	518.7	519.7	520.6
Residue weight at 800 °C (W ₈₀₀ , %)	60.1	62.3	64.2	66.1	68.2
Tensile strength (MPa)	107.4	93.1	86.8	79.5	75.7
Tensile modulus (MPa)	2038	1825	1692	1640	1596
Elongation at break (%)	12.47	9.45	7.19	5.61	4.78
Dielectric constant at 1000 Hz (ε _r)	3.96	4.34	4.5	4.61	4.72
Breakdown strength (E _b , kV/mm)	227.5	212.7	207.2	202.1	197.3
Discharged energy density (U _d , J/cc)	0.56	0.60	0.62	0.62	0.63
Discharged energy efficiency (η, %)	98.4	97.5	96.2	94.8	93.3

Table S2. Properties of TiO₂-PEN hybrids.

	0 wt%	5 wt%	10 wt%	15 wt%	20 wt%
Glass transition temperature (T _g , °C)	217.7	217.9	218.1	220.4	221.7
Decomposition temperature (T _{10%} , °C)	521.7	531.2	539.1	547.1	560.9
Residue weight at 800 °C (W ₈₀₀ , %)	66.3	67.9	69.6	71.4	73.1
Tensile strength (MPa)	109.7	115.3	113.4	111.1	109.2
Tensile modulus (MPa)	2156	2277	2104	2059	1985
Elongation at break (%)	9.23	7.75	7.22	6.19	5.39
Dielectric constant at 1000 Hz (ε _r , 25 °C)	3.86	4.33	4.67	4.86	5.04
Breakdown strength (E _b , 25 °C, kV/mm)	224.8	212.4	204.8	199.4	194.3
Discharged energy density (U _d , 25 °C, J/cc)	0.53	0.59	0.63	0.65	0.65
Discharged energy efficiency (η, 25 °C, %)	96.5	95.4	94.3	92.9	91.3
Dielectric constant at 1000 Hz (ε _r , 150 °C)	4.07	4.49	4.79	4.96	5.09
Breakdown strength (E _b , 150 °C, kV/mm)	208.1	198.4	192.7	187.2	181.9
Discharged energy density (U _d , 150 °C, J/cc)	0.54	0.59	0.60	0.61	0.62
Discharged energy efficiency (η, 150 °C, %)	93.6	92.4	91.0	89.2	87.1

Table S3. Comparison of the composites characteristics with those in the literature.

Sample	ε_r	Tan δ	E_b (kV/mm)	η (%)	U_c (J/cm ³)	T_g (°C)	reference
TiO ₂ -PEN	5.04	0.021	194.3	91.3	0.84	221.7	This work
TiO ₂ /PEN	4.72	0.027	197.3	93.3	0.81	202.4	This work
CCTO/PEN	4.99	0.038	168.8	/	0.63	/	[1]
PENS100	3.60	0.018	203.5	/	0.68	180.0	[2]
TR-PEN200	4.11	0.020	220.7	/	0.89	222.9	[3]
CCTO15-PEN	6.27	0.027	162.4	/	0.78	/	[4]
PENK2	4.07	0.013	191.2	/	0.66	216.2	[5]
BT@CuPc/PEN	5.41	0.017	187.2	/	0.82	217.1	[6]
BT@PANI/PEN	4.55	0.013	208.5	/	0.78	216.4	[7]

References

- [1] F Gao, R Wei, L Zhou, W Luo, Z Li, L Pang, S Li, X Hua, L Wang, Improved dielectric properties of poly(arylene ether nitrile) with sulfonated poly(arylene ether nitrile) modified CaCu₃Ti₄O₁₂, Polym Compos, 2023, 44, 8658-8668.
- [2] W Hu, Y You, L Tong, L Tu, Y Wang, R Wei, X Liu. Preparation and physical properties of polyarylene ether nitrile and polyarylene ether sulfone random copolymers, High Perform Polym, 2018, 31, 686-693.
- [3] Y You, S Liu, L Tu, Y Wang, C Zhan, X Du, R Wei, X Liu. Controllable fabrication of poly(arylene ether nitrile) dielectrics for thermal-resistant film capacitors, Macromolecules, 2019, 52, 5850-5859.
- [4] L Zhou, Z Zhang, Y Feng, F Gao, Y Luo, S Li, R Wei, L Wang. Covalently cross-linked CaCu₃Ti₄O₁₂ and poly(arylene ether nitrile) hybrids with enhanced high temperature energy storage properties, Mater Today Commun, 2024, 38, 108544.
- [5] H Mao, Y You, L Tong, X Tang, R Wei, X Liu. Dielectric properties of deblock copolymers containing a polyarylene ether nitrile block and a polyarylene ether ketone block, J Mater Sci-Mater Electron, 2017, 29, 3127-3134.
- [6] Y You, W Han, L Tu, Y Wang, R Wei, X Liu. Double-layer core/shell-structured nanoparticles in polyarylene ether nitrile-based nanocomposites as flexible dielectric materials, RSC Adv 2017, 7, 29306-29311.
- [7] R Wei, Q Huo, K Liu, AY Elnaggar, SM El-Bahy, ZM El-Bahy, J Ren, L Wang, Z Wu. Distributing fluorinated carbon nanotube on pore walls of polyarylene ether nitrile porous films for advanced electromagnetic interference shielding, Adv Compos Hybrid Mater, 2024, 7, 196.